

ON THE CALCULATION OF THE TEMPERATURE FIELD IN SOLIDS WITH VARIABLE HEAT-TRANSFER COEFFICIENTS

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A method is presented for the approximate determination of the temperature field in solids with variable heat-transfer coefficients.

The mathematical formulation of the problem of the temperature field in a solid body with a variable heat-transfer coefficient is:

$$\frac{\partial \vartheta(\Psi, Fo)}{\partial Fo} = \frac{\partial^2 \vartheta(\Psi, Fo)}{\partial \Psi^2} + \frac{K-1}{\Psi} \frac{\partial \vartheta(\Psi, Fo)}{\partial \Psi}, \quad (1)$$

$$\partial \vartheta(1, Fo)/\partial \Psi = Bi(Fo) [1 - \vartheta(1, Fo)], \quad (2)$$

$$\partial \vartheta(0, Fo)/\partial \Psi = 0, \quad (3)$$

where

$$\vartheta(\Psi, 0) = \vartheta_0, \quad (4)$$

$$\vartheta = T/T_c, \quad 0 \leq \Psi \leq 1, \quad 0 \leq Fo = a\tau/R^2 < \infty,$$

Bi = $\alpha R/\lambda$, and the factor K is equal to 1, 2, or 3 in the plane, cylindrical, and spherical problem, respectively.

Introducing a new variable $\xi(\Psi, Fo)$, related to $\vartheta(\Psi, Fo)$ by

$$\xi(\Psi, Fo) = \ln[1 - \vartheta(\Psi, Fo)], \quad (5)$$

we may rewrite the system (1)-(4) in the form:

$$\frac{\partial \xi(\Psi, Fo)}{\partial Fo} = \frac{\partial^2 \xi(\Psi, Fo)}{\partial \Psi^2} + \frac{K-1}{\Psi} \frac{\partial \xi(\Psi, Fo)}{\partial \Psi} + \left[\frac{\partial \xi(\Psi, Fo)}{\partial \Psi} \right]^2, \quad (6)$$

$$\partial \xi(1, Fo)/\partial \Psi = -Bi(Fo), \quad (7)$$

$$\partial \xi(0, Fo)/\partial \Psi = 0, \quad (8)$$

$$\xi(\Psi, 0) = \ln(1 - \vartheta_0). \quad (9)$$

The quantity $(\partial \xi / \partial \Psi)^2$ in (6) increases monotonically from zero at $\Psi = 0$ to a maximum value at $\Psi = 1$, and can be regarded from the physical point of view as an internal heat source of variable strength. Being a function of Fo and Bi, this quantity decreases with decreasing Bi and becomes negligibly small for $Bi \leq 0.25$ ("thin" body). Assuming $(\partial \xi / \partial \Psi)^2 = 0$, using the solutions of the system (6)-(9), and taking account of (5), we obtain the required temperature distribution.

Infinite plate:

$$\begin{aligned} \vartheta(x/R, Fo) = & 1 - \exp \left\{ \ln(1 - \vartheta_0) - \int_0^{Fo} Bi(Fo) dFo + \right. \\ & + \frac{1}{6} Bi(Fo) [1 - 3(x/R)^2] - \sum_{n=1}^{\infty} (-1)^{n+1} \frac{2}{\mu_n^2} \cos \mu_n \frac{x}{R} \exp(-\mu_n^2 Fo) \times \\ & \left. \times \int_0^{Fo} \exp(\mu_n^2 Fo) Bi'(Fo) dFo \right\}. \end{aligned} \quad (10)$$

Infinite cylinder:

$$\begin{aligned} \vartheta(r/R, Fo) = & 1 - \exp \left\{ \ln(1 - \vartheta_0) - 2 \int_0^{Fo} Bi(Fo) dFo + \right. \\ & + \frac{1}{4} Bi(Fo) [1 - 2(r/R)^2] - \sum_{n=1}^{\infty} \frac{2}{\mu_n^2 J_0(\mu_n)} J_0(\mu_n r/R) \times \\ & \left. \times \exp(-\mu_n^2 Fo) \int_0^{Fo} \exp(\mu_n^2 Fo) Bi'(Fo) dFo \right\}. \end{aligned} \quad (11)$$

Sphere:

$$\begin{aligned} \vartheta(r/R, Fo) = & 1 - \exp \left\{ \ln(1 - \vartheta_0) - 3 \int_0^{Fo} Bi(Fo) dFo + \right. \\ & + \frac{1}{10} Bi(Fo) [3 - 5(r/R)^2] - \sum_{n=1}^{\infty} \frac{2}{\mu_n^2 \cos \mu_n} \frac{R \sin \mu_n r/R}{r \mu_n} \times \\ & \left. \times \exp(-\mu_n^2 Fo) \int_0^{Fo} \exp(\mu_n^2 Fo) Bi'(Fo) dFo \right\}. \end{aligned} \quad (12)$$

It can be easily seen that the expressions (10)-(12) are exact solutions of Eq. (1) with boundary conditions (2)-(4) at the point $\psi = 0$.

Temperature Field in an Infinite Plate for $\vartheta_0 = 0.336$

Fo	$\vartheta_{\text{surface}}$			$\vartheta_{\text{center}}$		
	according to (10)	according to the finite-difference method	$\delta, \%$	according to (10)	according to the finite-difference method	$\delta, \%$
0.5	0.5560	0.5257	-5.83	0.3971	0.4004	-0.827
1.0	0.7143	0.6777	-5.41	0.5691	0.5379	-5.800
1.5	0.8135	0.7693	-5.75	0.7016	0.6619	-6.000
2.0	0.8983	0.8473	-5.99	0.8151	0.7703	-5.810
2.5	0.9275	0.8834	-5.00	0.8779	0.8333	-5.350
3.0	0.9543	0.9210	-3.62	0.9281	0.8781	-5.680
3.5	0.9764	0.9465	-3.15	0.9555	0.9172	-4.180
4.0	0.9902	0.9640	-2.71	0.9822	0.9441	-4.040

Numerical calculations according to [1] show that the error of Eqs. (10)-(12) does not exceed 6% over the whole range of variation of ψ for $Bi \leq 1.2$ (infinite plate), $Bi \leq 1.35$ (infinite cylinder), or $Bi \leq 1.5$ (sphere). The accuracy of the calculation increases with decreasing Bi .

As an example, we have calculated the heating of an infinite plate when the Biot number varies according to the law $Bi(Fo) = 1.2 - \exp(-Fo)$ (cf. table.).

Thus Eqs. (10)-(12) can be used for an approximate calculation of the temperature field when $Bi = Bi(Fo)$.

REFERENCE

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